



# Low-temperature selective catalytic reduction of NO with NH<sub>3</sub> over monolith catalyst of MnO<sub>x</sub>/CeO<sub>2</sub>-ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>

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## ABSTRACT

MnO<sub>x</sub>/CeO<sub>2</sub>-ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> (MnO<sub>x</sub>/CZA) catalysts with different amounts of manganese loading were prepared by incipient wetness impregnation method for selective catalytic reduction (SCR) of NO with NH<sub>3</sub> at low temperature. The catalysts were characterized by N<sub>2</sub> adsorption-desorption measurement, XRD, XPS, and H<sub>2</sub>-TPR. Catalytic activity tests reveal that the MnO<sub>x</sub>/CZA catalyst with 10% manganese loading has the best catalytic activity, almost 90% NO is translated to N<sub>2</sub> in the temperature range of 143–300 °C. The highly dispersed MnO<sub>x</sub> species, the good oxidation activity of NO to NO<sub>2</sub>, the existent synergistic effect between the manganese and cerium oxides, and the various oxidation states of manganese oxides may be the main reasons for the best SCR activity. In addition, the SCR activity is slightly influenced in the presence of SO<sub>2</sub> and H<sub>2</sub>O, while such effect is restorable after heating treatment.

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## 1. Introduction

Nitrogen oxides from the combustion of fossil fuels are the main source of air pollution, and they contribute to acid rain, photochemical smog and ozone depletion. Currently, selective catalytic reduction (SCR) of NO<sub>x</sub> with NH<sub>3</sub> in the presence of excessive O<sub>2</sub> has been widely applied to reduce the emission of nitrogen oxides for its low cost and high efficiency [1]. As the most prevalent commercial catalyst, V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/TiO<sub>2</sub> exhibits high activity. But this catalyst is only active in a narrow temperature window of 300–400 °C [2,3]. Consequently, a highly efficient low-temperature SCR catalyst is often desired to avoid the reheating of flue gas and the deactivation caused by SO<sub>2</sub> and dust presented in the flue gas of stationary source. This catalyst can be located downstream of the equipment of desulfurizer and particle removal without preheating the flue gas.

In recent years, the Mn-based catalysts have been found to be highly effective for low temperature SCR of NO with NH<sub>3</sub>, and TiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub> and active carbon have been widely used as the support of the low temperature SCR catalyst [4–10]. In some studies, CeO<sub>2</sub> has been used to promote the SCR activity due to its ability of creating surface and bulk oxygen vacancies by generation Ce<sup>3+</sup>/Ce<sup>4+</sup> redox couples. The surface and bulk oxygen vacancies can promote the oxidation of NO to NO<sub>2</sub>, which will increase the catalytic activity for SCR of NO with NH<sub>3</sub> [11,12]. However, the specific surface

area of CeO<sub>2</sub> is not large enough, and its ability of creating surface and bulk oxygen vacancies needs to be improved. As a new generation oxygen-storage material, CeO<sub>2</sub>-ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> (CZA) is widely used in three-way catalysts [13–15]. CZA has potential application in NH<sub>3</sub>-SCR catalyst for its high thermal stability, high surface area and fine ability of creating surface and bulk oxygen vacancies. It is well-known that the monolith catalyst is more representative in catalysis application for its low pressure drop, short diffusion distances and large geometric surface area [16]. In this study, monolith MnO<sub>x</sub>/CZA catalysts with different manganese loadings were prepared and they were characterized by N<sub>2</sub> adsorption-desorption measurement, XRD, XPS and H<sub>2</sub>-TPR.

## 2. Experimental

### 2.1. Preparation of supports and catalysts

CeO<sub>2</sub>-ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> (CZA) and TiO<sub>2</sub> were prepared by coprecipitation method. To prepare CZA support, a mixture of Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O, ZrCO<sub>3</sub>·nH<sub>2</sub>O, and Al(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O in a molar ratio of 3:3:4 was dissolved in distilled water. The mixed aqueous solution of ammonia and (NH<sub>4</sub>)<sub>2</sub>CO<sub>3</sub> was used as the precipitator and was added dropwise to the metal salt solution. The resulting precipitates were aged, filtered, washed, and dried at 110 °C overnight, and then they were calcined at 600 °C for 3 h. TiO<sub>2</sub> was prepared under the similar conditions as used for CZA support, except that TiOSO<sub>4</sub>·2H<sub>2</sub>O was used as the metal salt and it was calcined at 500 °C for 3 h.

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MnO<sub>x</sub>/CZA catalysts with different manganese loadings were prepared by impregnating the CeO<sub>2</sub>-ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> powder with Mn(CH<sub>3</sub>COO)<sub>2</sub>·2H<sub>2</sub>O aqueous solution. Then the samples were dried at 105 °C overnight and calcined at 500 °C for 3 h. The resulting powders were subsequently coated on honeycomb cordierites (2.5 cm<sup>3</sup>, Yi Xing, China) and calcined at 500 °C for 3 h in air. The washcoat loading was about 180 g/L. These MnO<sub>x</sub>/CZA catalysts containing 5 wt.%, 10 wt.%, 15 wt.%, 20 wt.% and 30 wt.% manganese are referred as Cat-A, Cat-B, Cat-C, Cat-D and Cat-E.

MnO<sub>x</sub>/TiO<sub>2</sub> catalyst with 10% manganese loading (denoted as Cat-O) was prepared under the similar conditions as used for MnO<sub>x</sub>/CZA catalysts. The pure MnO<sub>x</sub> was prepared by calcination of Mn(CH<sub>3</sub>COO)<sub>2</sub>·2H<sub>2</sub>O at 500 °C for 3 h and then coated on honeycomb cordierites and calcined at 500 °C for 3 h in the air.

## 2.2. Characterization of the catalysts

BET surface area measurement was carried out on QUADRASORB SI automatic surface analyzer (Quantachrome Corporation). The samples were evacuated for 3 h at 300 °C, and then cooled to -196 °C using liquid N<sub>2</sub> at which point N<sub>2</sub> adsorption was measured.

Powder X-ray diffraction (XRD) data were collected on Rigaku D/MAX-rA diffractometer with Cu radiation ( $\lambda = 0.15406$  nm). The X-ray tube was operated at 45 kV and 25 mA. The samples were investigated in the  $2\theta$  range of 10–90° at a scanning speed of 0.03° S<sup>-1</sup>.

The H<sub>2</sub>-temperature programmed reduction (H<sub>2</sub>-TPR) was carried out in a quartz U-tube, and 100 mg sample was employed for each measurement. The sample was first pre-treated in N<sub>2</sub> (30 ml min<sup>-1</sup>) at 450 °C for 1 h and then cooled to room temperature. After that, a flowing H<sub>2</sub> (5% in N<sub>2</sub>, 30 ml min<sup>-1</sup>) was switched on with a linear heating rate of 8 °C min<sup>-1</sup>. A thermal conductivity cell was used to detect the consumption of H<sub>2</sub>.

XPS experiments were carried out on a spectrometer (XSAM-800, KRATOS Co.) with Al K $\alpha$  radiation under UHV. The C 1s peak (284.8 eV) was used for the calibration of binding energy values. The pressure in the analytical chamber was about 10<sup>-9</sup> Pa.

## 2.3. Catalytic activity measurements

The catalytic activity measurement was carried out in a fixed-bed quartz flow reactor. Reactant gases were regulated by means of mass-flow controllers before entering reactor. The concentration of simulated gases were as follow: 1000 ppm NO, 1000 ppm NH<sub>3</sub>, 5% O<sub>2</sub>, 10% water vapor (when used), 100 ppm SO<sub>2</sub> (when used), balance Ar, the gas hourly space velocity (GHSV) = 10,000 h<sup>-1</sup>, the total flow rate was 416 ml min<sup>-1</sup>. The water vapor was generated by passing Ar flow through a gas-wash device containing de-ionized water. The NO and NO<sub>2</sub> concentrations in the inlet and outlet gases were continually analyzed by a chemiluminescent NO/NO<sub>x</sub> analyzer (Model 42i, Thermo Electron Corporation). To avoid the influence caused by the oxidation of ammonia, the outlet stream was passed through an ammonia trap containing phosphoric acid solution before entering the chemiluminescent analyzer. The catalysts were pre-treated in Ar at 500 °C for 1 h before activity test.

The catalytic oxidation activities for NO to NO<sub>2</sub> were also measured. The reaction conditions were as follow: 1000 ppm NO, 5% O<sub>2</sub>, balance Ar, GHSV = 10,000 h<sup>-1</sup>. The conversion of NO to NO<sub>2</sub> was obtained by this equation: Conversion of NO to NO<sub>2</sub> = 100% × ([NO<sub>x</sub>]inlet - [NO]outlet)/[NO<sub>x</sub>]inlet, where NO<sub>x</sub> represents NO + NO<sub>2</sub>.

**Table 1**  
BET surface area, pore volume and pore size of CZA and MnO<sub>x</sub>/CZA catalysts.

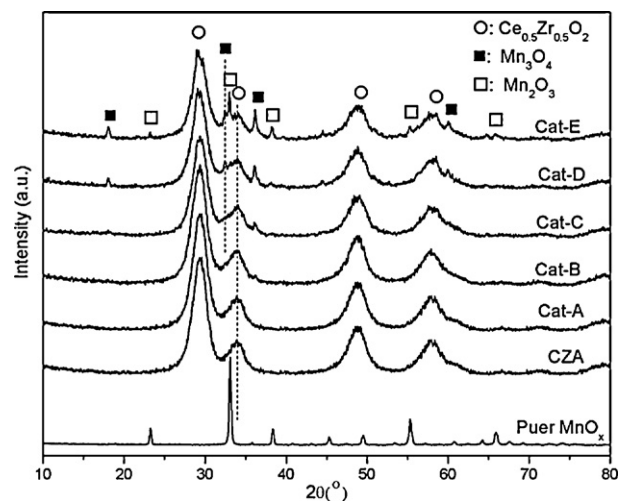
Samples	BET surface area (m <sup>2</sup> g <sup>-1</sup> )	Pore volume (cm <sup>3</sup> g <sup>-1</sup> )	Pore size (nm)
CZA	193	0.317	9.68
Cat-A	137	0.282	9.36
Cat-B	127	0.258	8.88
Cat-C	125	0.231	7.92
Cat-D	116	0.208	7.20
Cat-E	112	0.187	6.88

## 3. Results and discussion

### 3.1. Nitrogen adsorption and XRD

The BET surface area, pore volume, and pore size of various samples are summarized in Table 1. From Table 1, we can see that the specific surface area (193 m<sup>2</sup> g<sup>-1</sup>), pore volume (0.32 cm<sup>3</sup> g<sup>-1</sup>) and pore size (9.6 nm) of the CZA support are the largest among all of the samples. With the increase of manganese loading, a decrease of BET surface area, pore volume and pore size is observed. This can be easily understood by the fact that the free pore of CZA support is partially occupied by the manganese oxides.

XRD patterns of pure MnO<sub>x</sub> and MnO<sub>x</sub>/CZA with different manganese content are shown in Fig. 1. The diffraction peaks of pure MnO<sub>x</sub> are characteristic of Mn<sub>2</sub>O<sub>3</sub>, no other manganese oxides diffraction peaks are observed. It is noteworthy that the XRD patterns of MnO<sub>x</sub>/CZA catalysts and CZA presented here reveal no visible Al<sub>2</sub>O<sub>3</sub> diffraction peaks except for the distinct cubic fluorite-type phase diffraction peaks of Ce<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2</sub>. Although large amounts of Al<sub>2</sub>O<sub>3</sub> (40 wt.%) exist in CZA, not any Al<sub>2</sub>O<sub>3</sub> diffraction peaks are observed from XRD patterns. Thus the Al<sub>2</sub>O<sub>3</sub> in CZA forms solid solution accompany with Ce<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2</sub> solid solution more likely. This result shows that CZA forms homogeneous solid solutions and the Al<sub>2</sub>O<sub>3</sub> disperses well in CZA solid solutions. At low manganese loadings ( $\leq 10\%$ ), no manganese oxide diffraction peaks can be found. This may be due to the highly dispersed manganese oxide on CZA, or the amorphous phase of manganese oxide has formed on the surface of catalyst. As the manganese content increases, the crystal phase of Mn<sub>3</sub>O<sub>4</sub> becomes apparent, and the visible crystal phase of Mn<sub>2</sub>O<sub>3</sub> is also detected when the manganese loading reaches 30%. From the XRD results, it can be concluded that the manganese oxides disperse well on the MnO<sub>x</sub>/CZA with



**Fig. 1.** XRD patterns of MnO<sub>x</sub>/CZA catalysts with different manganese loading. Cat-A, Cat-B, Cat-C, Cat-D and Cat-E denote as MnO<sub>x</sub>/CZA with 5%, 10%, 15%, 20% and 30% manganese loading, respectively.

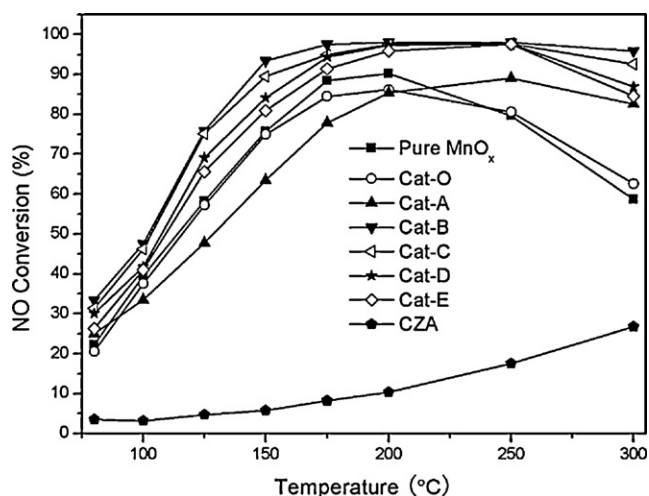


Fig. 2. NO conversion on different catalysts. Reaction conditions: total flow rate:  $416 \text{ ml min}^{-1}$ , 1000 ppm NO, 1000 ppm  $\text{NH}_3$ , 5%  $\text{O}_2$  and Ar balance, GHSV =  $10,000 \text{ h}^{-1}$ .

10% manganese content. Otherwise, the strong interaction between  $\text{MnO}_x$  and CZA induces the translating of  $\text{Mn}_2\text{O}_3$  oxidation state to various oxidation states of manganese oxides in  $\text{MnO}_x/\text{CZA}$  catalysts.

### 3.2. Catalytic performance

The catalytic activities of various catalysts for low-temperature SCR at a gases space velocity of  $10,000 \text{ h}^{-1}$  as a function of reaction temperature are shown in Fig. 2. It can be seen that the highest conversion of NO over the pure  $\text{MnO}_x$  and Cat-O monolith catalyst is below 85%, and they have a narrow activity temperature window of  $160\text{--}250^\circ\text{C}$  (NO conversion  $>80\%$ ). The CZA exhibits more inferior NO conversion, the highest conversion of NO is only 26.7%, and almost no NO conversion is obtained at low temperature ( $80\text{--}150^\circ\text{C}$ ). In comparison,  $\text{MnO}_x/\text{CZA}$  series catalysts are highly active at low temperature. As shown in Fig. 2, the NO conversion shows an evident upward trend with the increase of manganese loading until the manganese content reaches 10%. After this level, a further increase of manganese loading does not increase the activity. It can be seen that the catalyst with 5% manganese content exhibits inferior SCR activity, which may be caused by the lacking of enough active sites. The catalyst with 10% manganese loading

has the lowest light-off temperature (NO conversion is 50%) and the widest activity temperature window. It is light-off at  $103^\circ\text{C}$ , which is much lower than that of other catalysts. In the temperature range of  $143\text{--}300^\circ\text{C}$ , almost 90% NO conversion is presented over Cat-B. This is much better than those monolith catalysts reported in Refs. [8,9]. Considering the XRD results, it can be concluded that the finely dispersed manganese oxide on CZA is the main contribution to the SCR activity. With the increase of manganese loading, the highly dispersed  $\text{MnO}_x$  species may aggregate and the appearance of crystalline manganese oxide decreases the SCR activity.

### 3.3. The oxidation activity of NO to $\text{NO}_2$

Taking account of NO can be oxidized to  $\text{NO}_2$  in the presence of excessive  $\text{O}_2$ , the conversion of NO to  $\text{NO}_2$  in the absence of catalyst was measured with different concentrations of NO. As shown in Fig. 3(a), there are only a few conversions of NO to  $\text{NO}_2$  in the absence of catalyst. The lower concentrations of NO exhibit better oxidation activity of NO to  $\text{NO}_2$ . When the concentrations of NO are 200 ppm, the conversion of NO to  $\text{NO}_2$  is the highest, which is 3.8% at  $300^\circ\text{C}$ . The conversions of NO to  $\text{NO}_2$  gradually decrease with the increase of NO concentrations. Otherwise, with the increasing of temperature in the range of  $80\text{--}300^\circ\text{C}$ , the conversions of NO to  $\text{NO}_2$  increase. Thus it can be seen that the oxidation activity of NO to  $\text{NO}_2$  is very low in the absence of catalyst.

The conversions of NO to  $\text{NO}_2$  as a function of reaction temperature in excess oxygen over  $\text{MnO}_x$ , Cat-O and Cat-B catalysts are shown in Fig. 3(b). It is obvious that the introduction of the catalyst increases the oxidation activity of NO to  $\text{NO}_2$ . However, the oxidation activity of NO to  $\text{NO}_2$  on  $\text{MnO}_x$  and Cat-O is still low, especially at lower temperature. At  $100^\circ\text{C}$ , there are only 2.1% and 1.8% conversions over  $\text{MnO}_x$  and Cat-O, respectively. After  $\text{MnO}_x$  supporting on CZA oxygen storage material, the NO oxidation activity increases significantly, and the conversion over Cat-B catalyst is 4.6% at  $100^\circ\text{C}$  and 13.3% at  $150^\circ\text{C}$ . It has been established that NO is more readily reduced to  $\text{N}_2$  along with portion  $\text{NO}_2$  than single NO by ammonia [17,18]. It can be seen from Fig. 3(b), the introduction of CZA oxygen storage material increases the oxidation rate of NO to  $\text{NO}_2$ , which increases the SCR activity.

### 3.4. XPS analysis

To understand the surface properties of  $\text{MnO}_x/\text{CZA}$  catalysts, XPS studies were carried out. As shown in Fig. 4 and Table 2, a significant increase in the intensity and sharpening of Mn 2p peaks can be

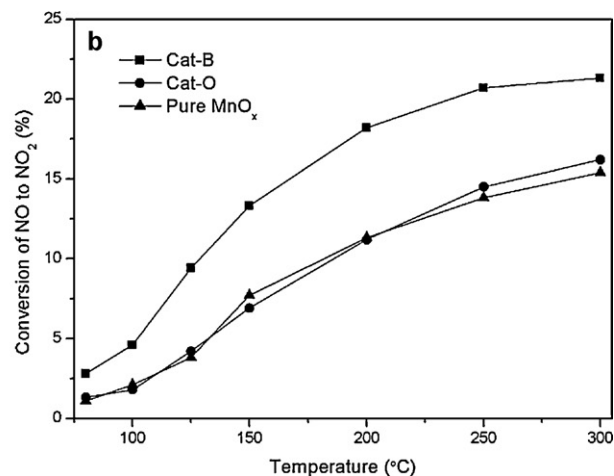
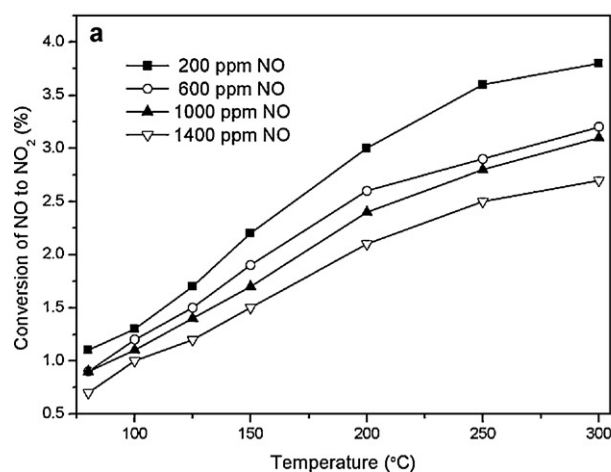


Fig. 3. (a) Oxidation activity of NO to  $\text{NO}_2$  by  $\text{O}_2$  in the absence of catalyst. Reaction conditions: 200 ppm, 600 ppm, 1000 ppm or 1400 ppm NO, 5%  $\text{O}_2$  and Ar balance, GHSV =  $10,000 \text{ h}^{-1}$ . (b) Oxidation activity of NO to  $\text{NO}_2$  by  $\text{O}_2$  over  $\text{MnO}_x$ ,  $\text{MnO}_x/\text{TiO}_2$  and Cat-B. Reaction conditions: 1000 ppm NO, 5%  $\text{O}_2$  and Ar balance, GHSV =  $10,000 \text{ h}^{-1}$ .

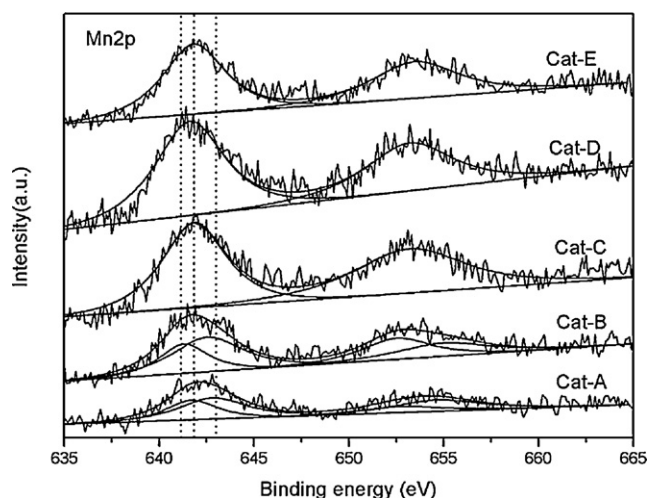


Fig. 4. Mn 2p XPS spectra of  $\text{MnO}_x/\text{CZA}$  catalysts.

observed with the increasing of Mn loading. It can be seen that there are two groups of Mn 2p fitting peaks in Cat-A and Cat-B, which can be explained due the presence of different oxidation states of Mn. The main peaks of the Mn  $2p_{3/2}$  level at higher BE value of 642.8 eV for Cat-A and 642.5 eV for Cat-B are attributed to the  $\text{Mn}^{4+}$  species of  $\text{MnO}_2$  [19,20]. The main peak at lower BE value of 641.7 eV in Cat-A is attributed to the  $\text{Mn}^{3+}$  species of  $\text{Mn}_2\text{O}_3$  [19–21]. For Cat-B, the lower BE value peak is shifted to 641.3 eV, which can be attributed to a mixed-valence of  $\text{Mn}^{3+}$  and  $\text{Mn}^{2+}$  cations within the surface of this catalyst. On the other hand, the BE value here also can be attributed to the  $\text{Mn}_3\text{O}_4$  species [19–22]. The BE values of  $\text{MnO}$  and  $\text{Mn}_2\text{O}_3$  are very close to each other, which causes difficulty in unambiguous identification of the oxidation state [19,20,22]. The Mn  $2p_{3/2}$  peaks in Cat-C, Cat-D and Cat-E have only one electronic binding energy peak, which is locate at 641.8, 641.6 and 641.8 eV, respectively. It is obvious that the Mn  $2p_{3/2}$  BE values of Cat-C, Cat-D and Cat-E are characteristic of  $\text{Mn}^{3+}$  species [19,20]. These results illustrates the presence of  $\text{MnO}_2$  as a major phase along with  $\text{Mn}_3\text{O}_4$  as the minor phase at lower loadings; but the  $\text{MnO}_2$  phase disappears at higher Mn loading.

Fig. 5 shows the Ce 3d XPS spectra of  $\text{MnO}_x/\text{CZA}$  catalysts. It can be seen that Ce 3d spectra are very complicated, which can be resolved into six components. The series of peaks denoted by “u” and “v” represent the Ce  $3d_{5/2}$  and the Ce  $3d_{3/2}$  states contribution, respectively. From these peaks,  $\text{Ce}^{4+}$  oxidation state is predominant, and  $\text{Ce}^{3+}$  oxidation state is indistinct identification through the Ce 3d spectra [19,23,24]. The peaks of u and u’ can be assigned to a mixing of  $3d^9 4f^2$  ( $O 2p^4$ ) and  $3d^9 4f^1$  ( $O 2p^5$ )  $\text{Ce}^{4+}$  final states, and u’’ to the  $3d^9 4f^0$  ( $O 2p^6$ )  $\text{Ce}^{4+}$  state. The series of v structures from the Ce  $3d_{3/2}$  states can be explained in the same way [24,25]. The u peak of Ce  $3d_{5/2}$  is locate at 882.0 eV for pure  $\text{CeO}_2$  [19]. As show in Table 2, the u peaks of Ce  $3d_{5/2}$  BE of  $\text{MnO}_x/\text{CZA}$  catalysts are apparently higher than that of pure  $\text{CeO}_2$ . Otherwise, the BE value of u gradually shifts to higher binding energy with the

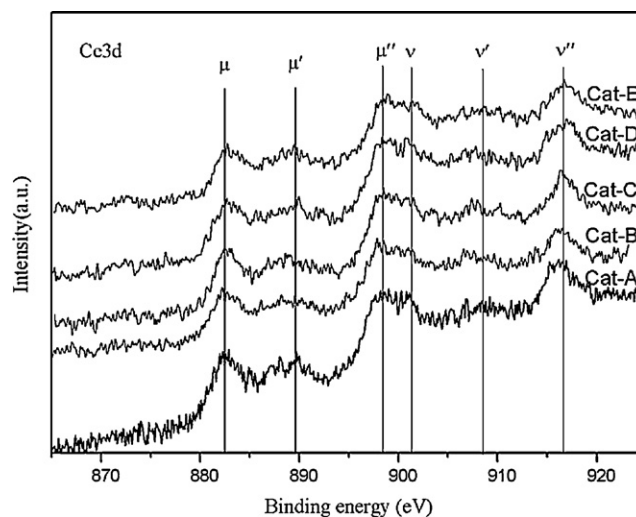


Fig. 5. Ce 3d XPS spectra of  $\text{MnO}_x/\text{CZA}$  catalysts.

increase of manganese content. It can be seen that the addition of  $\text{MnO}_x$  changes the surface chemical surrounding of Ce atom, and this indicates that strong interaction exists between Ce and other atoms.

As shown in Table 2, it can be observed that the increasing manganese content increases the molar percentage of Mn on the surface of catalyst until the manganese loading reached 20%, while the molar percentage of Ce decrease. However, when the manganese loading reaches 30%, the surface molar percentage of Mn decreases, and that of Ce increases. Furthermore, the  $\text{Mn}^{4+}/\text{Mn}$  2p molar ratio can be taken as a measure of the main active phase of manganese oxide on the catalyst surface (see Table 2). As can be noted, the molar ratio of  $\text{Mn}^{4+}/\text{Mn}$  2p is 58.8% in Cat-A and 62.9% in Cat-B, which indicates that the support surface is mainly covered by  $\text{MnO}_2$  at lower manganese loadings ( $\leq 10\%$ ). It is well known that the detection depth of XPS analysis is only 2 nm. Therefore, we suggest that the crystalline manganese oxides may agglomerate to nanometer particle with a size larger than 2 nm, and they may also insert into the pore structure of CZA. On the other hand, the excess Mn atoms may migrate into the bulk phase of Cat-E. All of the above suggestions cause the site of manganese exceeding the detection depth of XPS technique. It can be concluded that the  $\text{Mn}_3\text{O}_4$  phase detected by XRD in Cat-C, Cat-D and Cat-E exceed the detection depth of XPS testing.

Imamura et al. and Ding et al. suggested that a synergistic effect existed between the manganese and cerium oxides when simultaneous existing of  $\text{Mn}_2\text{O}_3$  and  $\text{CeO}_2$  [26,27]. Kapteijn et al. [28] suggested that the activity and selectivity of manganese oxide were obviously influenced by the oxidation state and the degree of crystallinity. The  $\text{Mn}_2\text{O}_3$  exhibited the highest selectivity for  $\text{N}_2$  while the  $\text{MnO}_2$  exhibited the highest activity. Therefore, it can be concluded that the existent synergistic effect between the manganese and cerium oxides may be a main contribution to the SCR activity

Table 2

Binding energy, surface molar percentage and relative area ratio of different manganese species determined from XPS and TPR.

Sample	Binding energy (eV)		Molar percentage		$\text{Mn}^{4+}/\text{Mn}$ (XPS, %)	Area ratio of $\text{Mn}^{4+} \rightarrow \text{Mn}^{3+}$ and $\text{Mn}^{3+} \rightarrow \text{Mn}^{2+}$ (TPR)
	Mn $2p_{3/2}$	Ce $3d_{5/2}$	Mn (%)	Ce (%)		
Cat-A	641.7; 642.8	882.5	1.89	4.81	58.8	4:2
Cat-B	641.3; 642.5	882.6	2.91	3.44	62.9	5:2
Cat-C	641.8	882.7	3.44	2.73	0	3:2
Cat-D	641.6	882.9	3.82	2.77	0	2:2
Cat-E	641.8	882.9	3.57	3.30	0	3:2



over  $\text{MnO}_x/\text{CZA}$  catalysts, and the various oxidation state of Mn in Cat-B may be another contribution to the excellent SCR activity.

### 3.5. $\text{H}_2$ -TPR study

The  $\text{H}_2$ -TPR was used in the present study to investigate the oxidation states of CZA support and  $\text{MnO}_x/\text{CZA}$  catalysts. The Gaussian fitting results of  $\text{H}_2$ -TPR are shown in Fig. 6, the CZA support shows a main reduction peak with the maximum at  $508^\circ\text{C}$  in the range of  $100\text{--}700^\circ\text{C}$ , indicating the reduction of surface  $\text{Ce}^{4+}$  to  $\text{Ce}^{3+}$  [29]. A very small shoulder is also observed in CZA around  $420^\circ\text{C}$ , which is assigned to the reduction of surface absorbed oxygen species. After  $\text{MnO}_x$  is supported on CZA, the reduction peaks of samples are obviously broadened. This suggests that the reducible manganese species exists in a mixed-valence such as  $\text{MnO}_2$ ,  $\text{Mn}_2\text{O}_3$  or  $\text{Mn}_3\text{O}_4$ , which is consistent with the results of XPS and XRD. The TPR profiles of Cat-A, Cat-B and Cat-C samples exhibit three reduction peaks. The reduction peak around  $360^\circ\text{C}$  is attributed to the reduction of  $\text{MnO}_2$  to  $\text{Mn}_2\text{O}_3$  and the reduction of surface absorbed oxygen species, and the reduction peaks at higher temperature of  $400\text{--}700^\circ\text{C}$  are assigned to the reduction of  $\text{Mn}_2\text{O}_3 \rightarrow \text{MnO}$  and the reduction of bulk phase absorbed oxygen species [30–32]. This reduction process has two types. The reduction peak around  $450^\circ\text{C}$  can be regarded as the reduction of  $\text{Mn}_2\text{O}_3$  to  $\text{Mn}_3\text{O}_4$  [30–32]. The reduction peak around  $480\text{--}600^\circ\text{C}$  should be assigned to the reduction of both  $\text{Mn}_3\text{O}_4$  to  $\text{MnO}$  and reducible surface  $\text{CeO}_2$  to  $\text{Ce}_2\text{O}_3$  [30–33]. For Cat-D and Cat-E, there are two hydrogen consumption peaks in the range of  $100\text{--}700^\circ\text{C}$ , the reduction peak around  $380^\circ\text{C}$  belongs to the reduction of  $\text{MnO}_2$  to  $\text{Mn}_3\text{O}_4$ , whereas the higher temperature peak represented the reduction of  $\text{Mn}_3\text{O}_4 \rightarrow \text{MnO}$ ,  $\text{Mn}_2\text{O}_3 \rightarrow \text{MnO}$  and easily reducible surface  $\text{CeO}_2$  to  $\text{Ce}_2\text{O}_3$  [30,31,34]. This indicates that the increased manganese loading may induce the reduction of  $\text{MnO}_2$  to  $\text{MnO}$  from three steps to two steps.

Fig. 6 indicates that the reduction temperature of  $\text{MnO}_2$  to  $\text{Mn}_2\text{O}_3$  over Cat-B is lower than that of the other catalysts, which illustrates that the  $\text{MnO}_x$  on Cat-B is more active than the other catalysts. This indicates that the lower reduction temperature represents the higher dispersion of  $\text{MnO}_x$  over the surface of CZA. When the manganese loading exceeds 10%, the reduction temperature of  $\text{MnO}_2$  gradually shifts towards higher temperature with

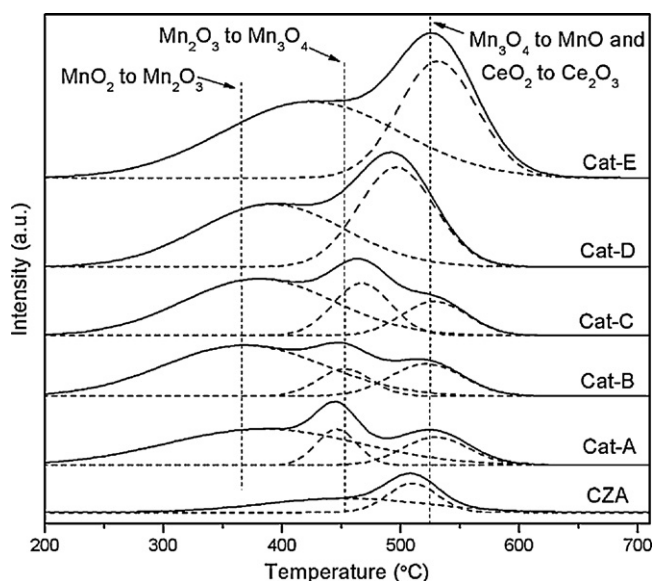


Fig. 6. The  $\text{H}_2$ -TPR profiles of CZA and  $\text{MnO}_x/\text{CZA}$  catalysts.

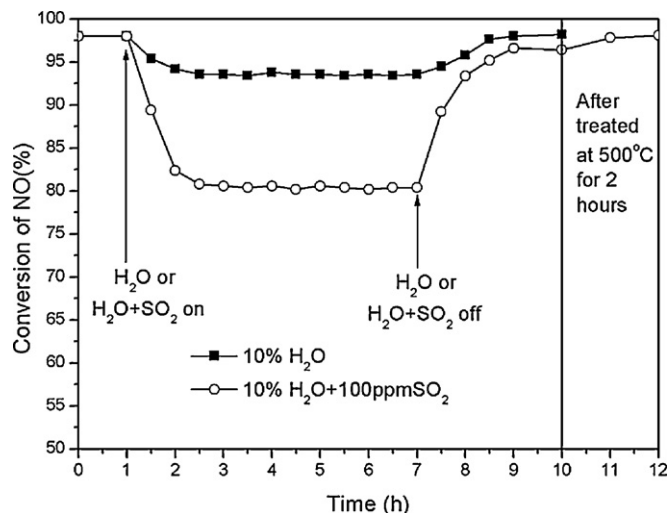


Fig. 7. The effects of  $\text{H}_2\text{O}$  and  $\text{SO}_2$  on the SCR activity of Cat-B catalyst. Reaction conditions:  $416\text{ ml min}^{-1}$  total flow rate, 1000 ppm NO, 1000 ppm  $\text{NH}_3$ , 5%  $\text{O}_2$ , 10%  $\text{H}_2\text{O}$  (when used), 100 ppm  $\text{SO}_2$  (when used) and Ar balance,  $200^\circ\text{C}$ , GHSV =  $10,000\text{ h}^{-1}$ .

increasing of manganese content. It is obvious that the finely dispersed manganese oxide decreases with the increase of manganese loading. But for Cat-A, there is only a weak shoulder peak for the reduction of highly dispersed surface  $\text{MnO}_x$ , which indicates that some free surface sites are not occupied by  $\text{MnO}_x$  species on the surface of CZA. The result is also supported by the XRD results mentioned in Fig. 1. When the manganese content reach 20%, the increased concentration of crystalline  $\text{Mn}_3\text{O}_4$  species in catalysts results in an enhanced intensity of the hydrogen consumption peak in the range of  $450\text{--}550^\circ\text{C}$ .

As shown in Table 2, the relative ratios of the reduction process of  $\text{MnO}_2 \rightarrow \text{Mn}_2\text{O}_3$  and  $\text{Mn}_2\text{O}_3 \rightarrow \text{MnO}$  are calculated from the  $\text{H}_2$  consumption during the TPR process. It can be seen that the majority of manganese species is  $\text{MnO}_2$  for all catalysts. The area ratio of the two step reduction process  $\text{MnO}_2 \rightarrow \text{Mn}_2\text{O}_3 \rightarrow \text{MnO}$  is calculated to be nearly 5:2 for Cat-B, which implied that the percentage of  $\text{MnO}_2$  species is the largest in Cat-B. Herein, the intermediate manganese species in the reduction of  $\text{MnO}_2 \rightarrow \text{Mn}_2\text{O}_3$  had similar oxidation state as that in  $\text{Mn}_2\text{O}_3$ . This clearly demonstrates that the  $\text{MnO}_2$  species is the mainly active species in  $\text{MnO}_x/\text{CZA}$  catalyst.

From the XRD results, it can be seen that no visible  $\text{MnO}_2$  diffraction peaks are observed in  $\text{MnO}_x/\text{CZA}$  catalysts. But from the XPS analysis, the oxidation state of  $\text{MnO}_2$  is detected only in Cat-A and Cat-B. The TPR results conclude that most of the manganese species might have stabilized as  $\text{Mn}^{4+}$  oxidation state on CZA. Furthermore, the activity results showed that the SCR activity of Cat-B is the best. The appearance of  $\text{Mn}_2\text{O}_3$  and  $\text{Mn}_3\text{O}_4$  crystal on Cat-C, Cat-D and Cat-E decreases the SCR activity, but the activity is still good. We suggest that  $\text{MnO}_2$ ,  $\text{Mn}_2\text{O}_3$  and  $\text{Mn}_3\text{O}_4$  are all active in  $\text{NH}_3$ -SCR reaction, but  $\text{MnO}_2$  is more active than that of  $\text{Mn}_2\text{O}_3$  and  $\text{Mn}_3\text{O}_4$  [11,28].

### 3.6. Effect of $\text{SO}_2$ and $\text{H}_2\text{O}$

Flue gases always contain small concentrations of  $\text{SO}_2$  and some concentrations of  $\text{H}_2\text{O}$ , even after desulphurization. It has been suggested that the coexistence of  $\text{SO}_2$  and  $\text{H}_2\text{O}$  has a serious poisoning effect on SCR activity at low temperature. Therefore, it is significant to investigate the effect of  $\text{H}_2\text{O}$  and  $\text{SO}_2$  on low-temperature SCR reaction. The effect of  $\text{H}_2\text{O}$  and  $\text{SO}_2 + \text{H}_2\text{O}$  on SCR activity over Cat-B catalyst is illustrated in Fig. 7. Before introducing 10%  $\text{H}_2\text{O}$  or 100 ppm

SO<sub>2</sub> + 10% H<sub>2</sub>O, the SCR reaction has stabilized for 1 h at 200 °C.

As shown in Fig. 7, when 10% H<sub>2</sub>O was added to the reaction gases, the NO conversion slightly decreases to about 93% from its original level, and then NO conversion almost stabilizes. After the removal of the water supply, the SCR activity increases and restores to its original level after 1.5 h. When 100 ppm SO<sub>2</sub> and 10% H<sub>2</sub>O were added to the reactants at 200 °C with a space velocity of 10,000 h<sup>-1</sup>, the NO conversion rapidly decreases to 80.4% from 98% in 1.5 h, and then nearly stabilizes. After turning off the SO<sub>2</sub> and H<sub>2</sub>O, the activity quickly restores to 96.4%. When the catalyst was heated for 2 h in Ar at 500 °C, the activity quickly restores to its initial level. This indicates that the Cat-B is resistant to water vapor and the mixture of H<sub>2</sub>O and SO<sub>2</sub> at 200 °C. The decreased activity in the process is mainly caused by the competing adsorption of H<sub>2</sub>O, SO<sub>2</sub> and reaction gases on the catalyst. It is clear that a small portion of tightly adsorbed SO<sub>2</sub>, the formed sulfates, and the ammonium sulfates on the catalyst surface occupy the active sites of catalyst, which consequently lead to the decrease of SCR activity [35,36]. After a heating treatment, the adsorbed SO<sub>2</sub> desorbs from the catalyst surface and the formed sulfates and ammonium sulfates decompose into SO<sub>x</sub> (SO<sub>2</sub> or SO<sub>3</sub>) and NH<sub>3</sub>, which is taken away by the blowing gas, so the SCR activity restores to its original level.

#### 4. Conclusions

The present work has shown that the MnO<sub>x</sub>/CZA monolithic catalysts are more active than pure manganese oxide and MnO<sub>x</sub>/TiO<sub>2</sub> catalysts for low-temperature SCR of NO with NH<sub>3</sub> in the presence of excess oxygen. The increases of manganese loading enhances the NO conversion of MnO<sub>x</sub>/CZA catalysts until manganese content up to 10%, and a further increase of manganese content decreases the SCR activity. The MnO<sub>x</sub>/CZA catalyst with 10% manganese loading presents the best catalytic activity for NO reduction. At higher manganese loading, the decreased activities of catalysts are caused by the formation of crystalline manganese oxides such as Mn<sub>3</sub>O<sub>4</sub> and Mn<sub>2</sub>O<sub>3</sub>. The superior SCR activity of MnO<sub>x</sub>/CZA catalyst with 10% manganese loading is due to the highly dispersed MnO<sub>x</sub> over CZA and the excellent oxidation activity of NO to NO<sub>2</sub>. At 10% manganese loading, the manganese oxides species presents various oxidation states such as MnO<sub>2</sub>, Mn<sub>3</sub>O<sub>4</sub> and MnO, and all of the manganese oxides species are highly dispersed or amorphous. The finely dispersed MnO<sub>2</sub> species is easily reduced at lower temperature in H<sub>2</sub>-TPR. This catalyst is also resistant to water vapor and the mixture of H<sub>2</sub>O and SO<sub>2</sub>.

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